

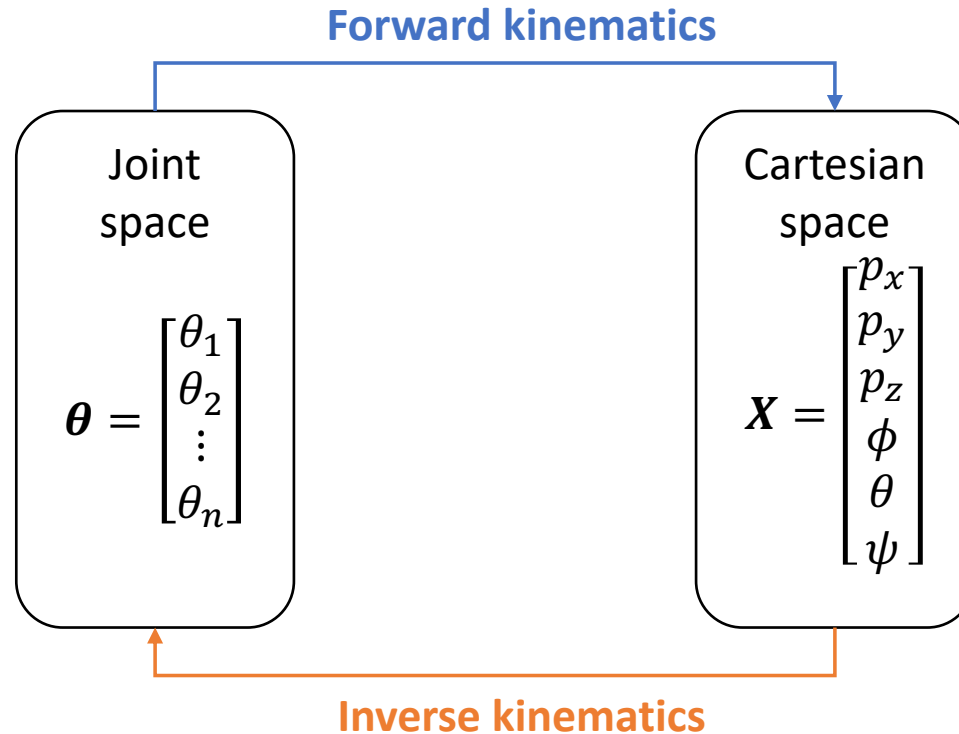
# ME729 Advanced Robotics - Inverse Kinematics

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# Inverse Kinematics

## □ Mappings between kinematic descriptions

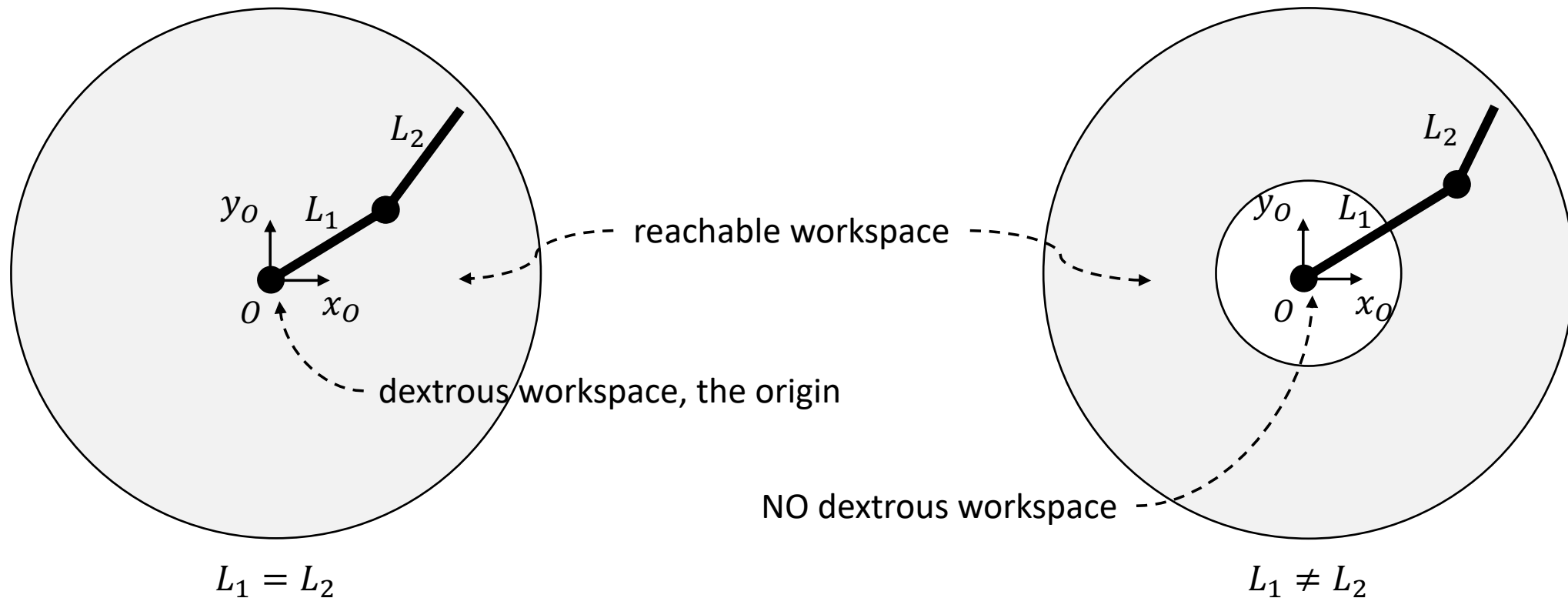


- Joint space: A set of  $n$  joint variables is referred to as the  $n \times 1$  joint vector. The space of all such joint vectors is referred to as joint space.
- Cartesian space: The term is used when position is measured along orthogonal axes, and orientation is measured to any of the conventions said before.

# Inverse Kinematics

## □ Existence of solutions

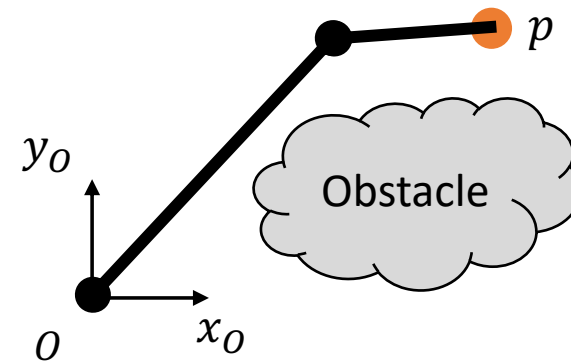
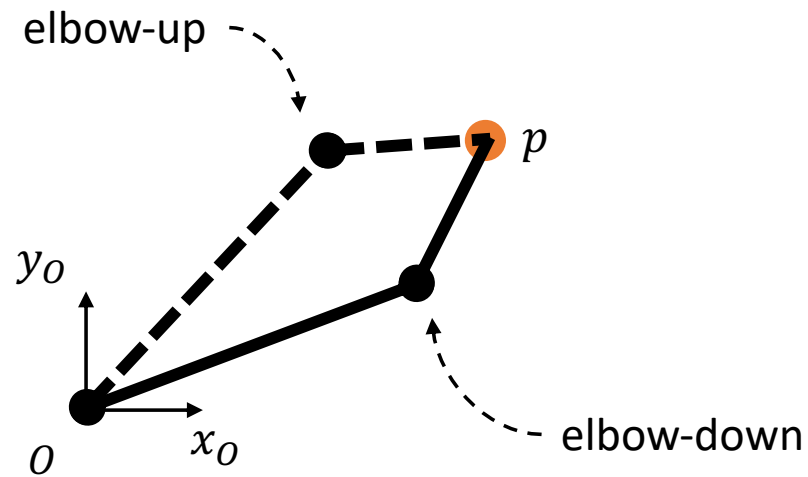
- Workspace: volume of space which **the end-effector of the manipulator can reach**.
- Dextrous workspace: volume of space which the robot end-effector can reach **with all orientation**.
- Reachable workspace: volume of space which the robot can reach **in at least one orientation**.
- For example, consider the two-link planar manipulator when  $L_1 = L_2$  and  $L_1 \neq L_2$ .



# Inverse Kinematics

## □ Multiple solutions

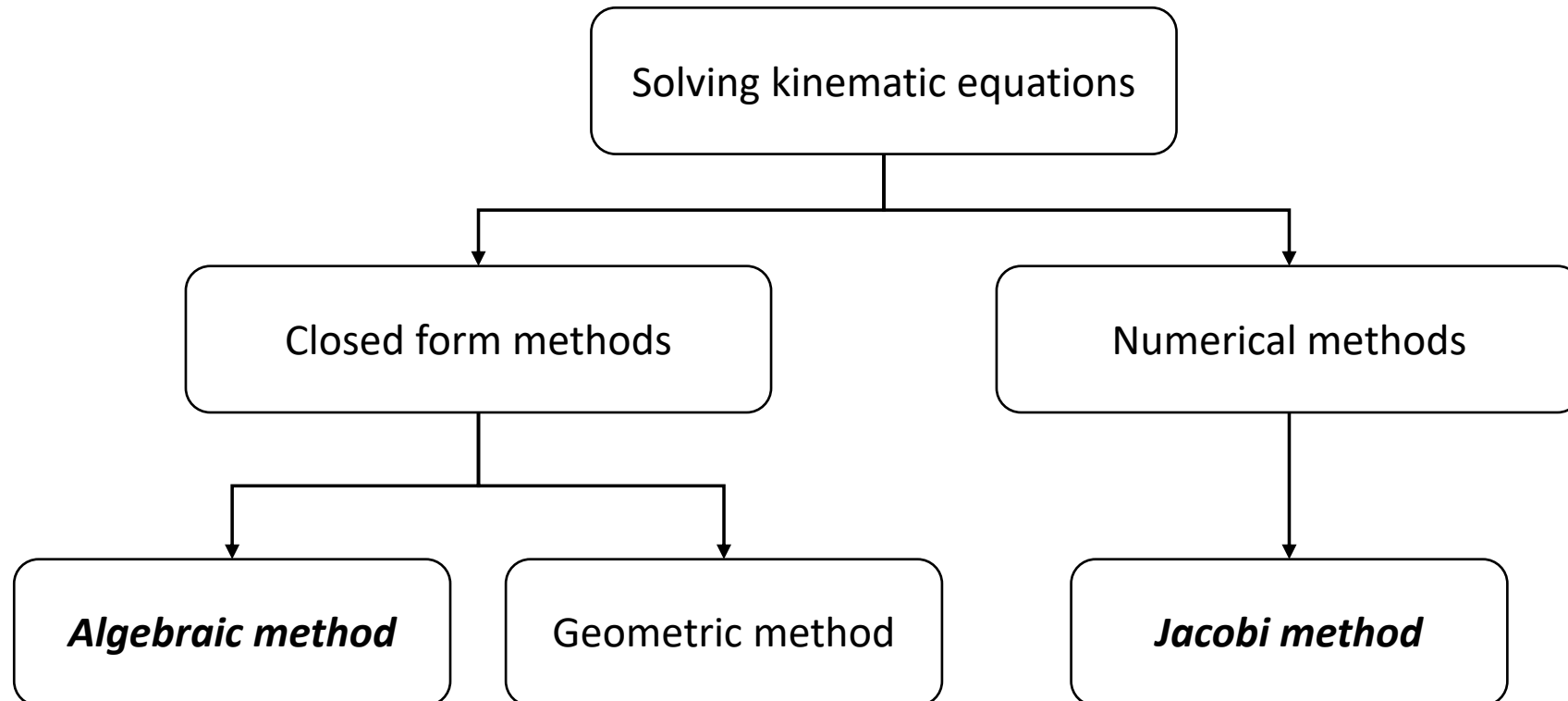
- When solving kinematic equations, we encounter multiple solutions.
- Let's see the two-link planar manipulator.
- To reach a point  $p$ , the robot can have two configurations: elbow up and down.
- In the present of the obstacle, the elbow up configuration would be chosen.



# Inverse Kinematics

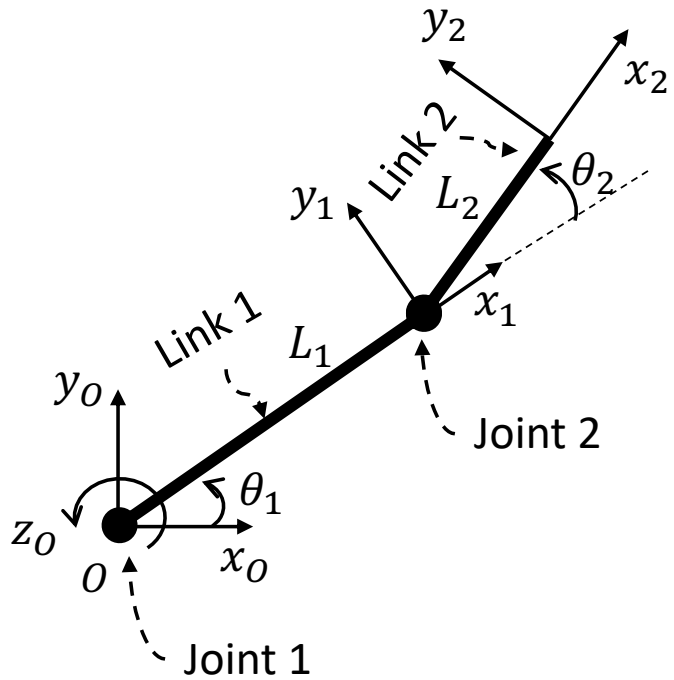
## □ Method of solution

- Closed form methods: based on analytic expressions.
- Numerical methods: based on iterative procedures.
- We consider two methods: **algebraic** and **Jacobi** method.



# Kinematic Equations

## □ The two-link planar manipulator



### 1) DH parameters table

$i$	$\theta_i$	$\alpha_i$	$a_i$	$d_i$	$\cos(\alpha_i)$	$\sin(\alpha_i)$
1	$\theta_1$	$0^\circ$	$L_1$	0	1	0
2	$\theta_2$	$0^\circ$	$L_2$	0	1	0

### 2) Link transformation matrices

$${}^0A_1 = \begin{bmatrix} c_1 & -s_1 & 0 & L_1c_1 \\ s_1 & c_1 & 0 & L_1s_1 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}, \quad {}^1A_2 = \begin{bmatrix} c_2 & -s_2 & 0 & L_2c_2 \\ s_2 & c_2 & 0 & L_2s_2 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$*\cos(\theta_i) = c_i, \sin(\theta_i) = s_i, \cos(\theta_i + \theta_j) = c_{ij}, \sin(\theta_i + \theta_j) = s_{ij}$$

### 3) The single transformation matrix that relates frame 2 from frame 0

$${}^0T_2 = \begin{bmatrix} c_1c_2 - s_1s_2 & -c_1s_2 - s_1c_2 & 0 & L_1c_1 + L_2c_1c_2 - L_2s_1s_2 \\ s_1c_2 + c_1s_2 & c_1c_2 - s_1s_2 & 0 & L_1s_1 + L_2s_1c_2 + L_2c_1s_2 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} c_{12} & -s_{12} & 0 & L_1c_1 + L_2c_{12} \\ s_{12} & c_{12} & 0 & L_1s_1 + L_2s_{12} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

# Algebraic Method

- From kinematic equations,  ${}^0A_1^{-1}{}^0T_2 = {}^1A_2$

$$\begin{bmatrix} c_1 & s_1 & 0 & -L_1 \\ -s_1 & c_1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} n_x & o_x & a_x & p_x \\ n_y & o_y & a_y & p_y \\ n_z & o_z & a_z & p_z \\ 0 & 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} c_2 & -s_2 & 0 & L_2c_2 \\ s_2 & c_2 & 0 & L_2s_2 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\begin{cases} p_x c_1 + p_y s_1 = L_2 c_2 + L_1 \\ -p_x s_1 + p_y c_1 = L_2 s_2 \end{cases}$$

- Square both equations and add them.

$$\begin{cases} p_x^2 c_1^2 + p_y^2 s_1^2 + 2p_x p_y c_1 s_1 = L_2^2 c_2^2 + L_1^2 + 2L_1 L_2 c_2 \\ p_x^2 s_1^2 + p_y^2 c_1^2 - 2p_x p_y c_1 s_1 = L_2^2 s_2^2 \end{cases}$$

$$p_x^2 + p_y^2 = L_2^2 + L_1^2 + 2L_1 L_2 c_2$$

$$\therefore c_2 = \frac{p_x^2 + p_y^2 - L_2^2 - L_1^2}{2L_1 L_2}$$

# Algebraic Method

- We write an expression for  $s_2$  as

$$s_2 = \pm \sqrt{1 - c_2^2}$$

$$\therefore \theta_2 = \text{atan2}(s_2, c_2)$$

- The choice of  $s_2$  signs corresponds to the multiple solution in which we can choose the 'elbow-down' or the 'elbow-up' solution.

- Remind these equations, 
$$\begin{cases} p_x c_1 + p_y s_1 = L_2 c_2 + L_1 \\ -p_x s_1 + p_y c_1 = L_2 s_2 \end{cases}$$

- Expressions for  $s_1$  and  $c_1$  are obtained by solving the equations.

$$\begin{cases} p_x p_y c_1 + p_y^2 s_1 = p_y (L_2 c_2 + L_1) \\ -p_x^2 s_1 + p_x p_y c_1 = p_x L_2 s_2 \end{cases}$$

$$(p_x^2 + p_y^2) s_1 = p_y (L_2 c_2 + L_1) - p_x L_2 s_2$$

$$\therefore s_1 = \frac{p_y (L_2 c_2 + L_1) - p_x L_2 s_2}{p_x^2 + p_y^2}$$

$$\begin{cases} p_x^2 c_1 + p_x p_y s_1 = p_x (L_2 c_2 + L_1) \\ -p_x p_y s_1 + p_y^2 c_1 = p_y L_2 s_2 \end{cases}$$

$$(p_x^2 + p_y^2) c_1 = p_x (L_2 c_2 + L_1) + p_y L_2 s_2$$

$$\therefore c_1 = \frac{p_x (L_2 c_2 + L_1) + p_y L_2 s_2}{p_x^2 + p_y^2}$$

$$\therefore \theta_1 = \text{atan2}(s_1, c_1)$$



# Jacobi Method

## □ Derive the Jacobian

- From kinematic equations,

$$\begin{cases} x_1 = f_1(\theta_1, \theta_2, \dots, \theta_n) \\ x_2 = f_2(\theta_1, \theta_2, \dots, \theta_n) \\ \vdots \\ x_n = f_n(\theta_1, \theta_2, \dots, \theta_n) \end{cases} \xrightarrow{\text{vector notation}} \mathbf{X} = f(\boldsymbol{\theta}),$$

where  $\mathbf{X}$  is a Cartesian space vector and  $\boldsymbol{\theta}$  is a joint space vector.

- Differentiate the kinematic equations.

$$\dot{\mathbf{X}} = \frac{\partial f}{\partial \boldsymbol{\theta}} \dot{\boldsymbol{\theta}} = \begin{bmatrix} f_1/\theta_1 & f_1/\theta_2 & \cdots & f_1/\theta_n \\ f_2/\theta_1 & f_2/\theta_2 & \cdots & f_2/\theta_n \\ \vdots & \vdots & \vdots & \vdots \\ f_n/\theta_1 & f_n/\theta_2 & \cdots & f_n/\theta_n \end{bmatrix} \dot{\boldsymbol{\theta}}$$

- Define the matrix of partial derivatives as the Jacobian,  $J(\boldsymbol{\theta})$ .

$$\therefore \dot{\mathbf{X}} = J(\boldsymbol{\theta})\dot{\boldsymbol{\theta}}$$

- If  $J(\boldsymbol{\theta})$  is invertible, we can calculate joint velocities given Cartesian velocities.

$$\dot{\boldsymbol{\theta}} = J(\boldsymbol{\theta})^{-1}\dot{\mathbf{X}}$$

# Jacobi Method

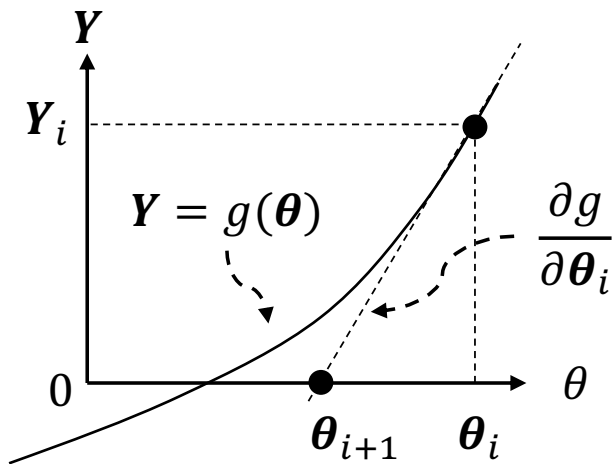
□ A way to find a solution of inverse kinematics

- When the desired Cartesian space,  $\mathbf{X}_d$ , the kinematic equation are rewritten as

$$\mathbf{X} - \mathbf{X}_d = f(\boldsymbol{\theta}) - \mathbf{X}_d$$

- Let  $\mathbf{X} - \mathbf{X}_d = \mathbf{Y}$  and  $f(\boldsymbol{\theta}) - \mathbf{X}_d = g(\boldsymbol{\theta})$ . Then  $\mathbf{Y} = g(\boldsymbol{\theta})$ .

- By **Newton-Rhapson method**, we can find the solution (i.e. the joint angles) satisfied with  $\mathbf{X}_d$ .



$$\frac{-Y_i}{\theta_{i+1} - \theta_i} = \frac{\partial g}{\partial \theta_i} = \frac{\partial f}{\partial \theta_i}$$

$$Y_i = \frac{\partial f}{\partial \theta_i} (\theta_i - \theta_{i+1})$$

$$\theta_{i+1} = -\frac{\partial f^{-1}}{\partial \theta_i} Y_i + \theta_i = \frac{\partial f^{-1}}{\partial \theta_i} (\mathbf{X}_d - \mathbf{X}_i) + \theta_i$$

$$\therefore \theta_{i+1} = J(\theta_i)^{-1} (\mathbf{X}_d - \mathbf{X}_i) + \theta_i$$

# Jacobi Method

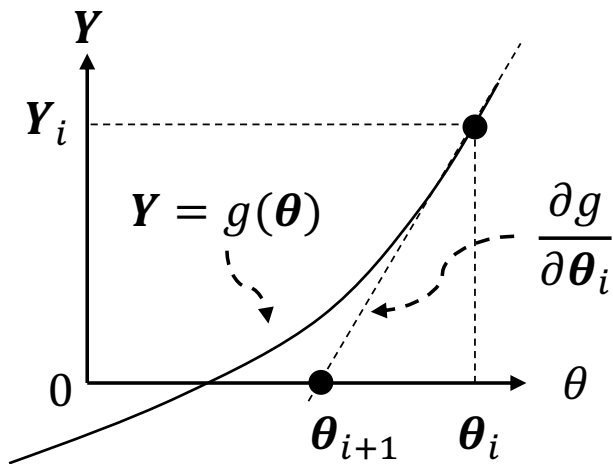
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- To remember easily, we rewrite the joint rates equation,  $\dot{\boldsymbol{\theta}} = J(\boldsymbol{\theta})^{-1}\dot{\mathbf{X}}$  as

$$\frac{\Delta \boldsymbol{\theta}}{\Delta t} = J(\boldsymbol{\theta})^{-1} \frac{\Delta \mathbf{X}}{\Delta t} \longrightarrow \Delta \boldsymbol{\theta} = J(\boldsymbol{\theta})^{-1} \Delta \mathbf{X}$$

$$\boldsymbol{\theta}_{i+1} - \boldsymbol{\theta}_i = J(\boldsymbol{\theta}_i)^{-1} (\mathbf{X}_d - \mathbf{X}_i)$$

$$\therefore \boldsymbol{\theta}_{i+1} = J(\boldsymbol{\theta}_i)^{-1} (\mathbf{X}_d - \mathbf{X}_i) + \boldsymbol{\theta}_i$$

# Jacobi Method

## □ Iteration flow

- Set initial guess  $\boldsymbol{\theta}_0$  and  $i = 0$ .
- Compute  $\mathbf{X}_0$  and  $J_0^{-1}$ .
- Check the error, i.e.  $\mathbf{X}_d - \mathbf{X}_0$  is less than a tolerance.
- If the error is less than the tolerance, terminate the iteration.
- If it isn't, compute  $\boldsymbol{\theta}_1 = J_0^{-1}(\mathbf{X}_d - \mathbf{X}_0) + \boldsymbol{\theta}_0$ .
- Increase  $i = 1$ , and update  $\boldsymbol{\theta}_i = \boldsymbol{\theta}_1$ .
- Keep iteration until the condition is satisfied.